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#### **Noise-based techniques for gas sensing**

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# Outline

- Introduction to noise and fluctuation-enhanced sensing (FES)
- Adsorption-desorption noise in gas sensors
  - Frequency and time domain response
- 1/f noise in gas sensors
- Higher order statistics
- Precautions
- Conclusions



# Introduction-general

[Bruschi& Sensors and

Actuators B, 19 (1994) 421]

#### • Electronic nose:

- arrays of N detectors with different selectivity for detection of M species (N>>M)
- Pattern recognition algorithms for selectivity
- Noise is considered as detrimental in sensing as it reduces the S/N ratio
- But noise is also a signal
- Fluctuation enhanced sensing (FES): [Kish&, Sensors and Actuators B, 71(2000)55]
  - employ patterns in noise characteristics of microfluctuations (e.g. spectra)
  - $\rightarrow$  reduction of number of sensing elements
  - In theory: one sensor could resolve mixture of gases





#### **Noise basics**





#### Adsorption / desorption (A/D) noise



#### **Adsorption / desorption (A/D) noise**



$$\tau = \frac{1}{\left(1/\tau_{ad} + 1/\tau_{des}\right)}$$

log(f)



**Spectral features:** 

corner frequency:  $f_{cor} = 1/(2\pi\tau)$ →multiple Lorenzians log(S) in a mixture of gases

 $- \tau_{ad} = f_{ad}(T, p_i, ...) \qquad \tau_{des} = f_{des}(T, p_i, ...)$ - f<sub>cor</sub> depends on temperature T and partial pressures p<sub>i</sub>

maximum amplitude of PSD occurs

for  $\tau_{ad} = \tau_{des} \rightarrow proper choise of T, p_i$ 



## Single adsorption/desorption events in graphene

- Exposure to low concentration of NO2
- Non-equilibrium situation (if equilibium  $\rightarrow$  RTS  $\rightarrow$



from [Shedin&, Nature, 6(2007)652]

LOGY

Quantized change in  $R(t) \xrightarrow{>} A/D$ 

0.3

0.1

# 1/f noise

Superposition of simple processes with Lorentzian spectra having a broad distribution of time constants: e.g. carrier number fluctuations



Complex scattering processes on defects and phonons: even a single scattering center can produce broadly distributed time constants



[Vandamme, Hooge I3E, TED 55(2008)3070]

#### **<u>1/f</u>** noise in gas sensor: correlation S<sub>R</sub>/R<sup>2</sup>(T) vs.



- Different Taguchi sensors (multigrain resistors)
- Temperature as control parameter
- power spectrum is not always correlated with changes in resistance [Solis& I3E Sens. J., 5(2005)1338]

 $\rightarrow$  1/f noise can be used for sensing too

$$\frac{S_R(T)}{R^2(T)} \approx R^m$$

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#### 1/f noise: selectivity of S<sub>R</sub>/R<sup>2</sup> (T) vs. gas



- temperature dependence of 1/f noise magnitude can give an information on selectivity in some sensors
- Additional info to R(T)

## Effect of humidity on 1/f noise in CuO NW



T=350°C, two-point configuration Relative humidity  $0\rightarrow$ 50% (RH50)

[Steinhauer&, APL, 107(2015)122112]



- Humidity increases the resistance due to "compensation" of the negative surface charge by the hydroxyl group [M.Huebner& Sens. Act. B 153(2011)347-53]

#### 1/f noise in CuO NW: effect of humidity



- 1/f noise found (no Lorentzians)
- Humidity increases the relative noise
- We consider mobility fluctuation model

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α-Hooge's noise coeff.
N-carrier number
μ-carrier mobility
q-element. charge
L - NW length

## 1/f noise in CuO NW: effect of humidity





Core/shell model s-surface b-bulk

Only surface resistance and surface noise changes due to gas are considered!!!

$$\frac{S_R}{R_{\text{TOT}}^2} = \frac{S_{Gs} + S_{Gb}}{G_{\text{TOT}}^2} = \frac{\frac{\alpha_s}{N_s f} G_s^2 + \frac{\alpha_b}{N_b f} G_b^2}{(G_s + G_b)^2} = \frac{K_s G_s + K_b G_b}{f L^2 (G_s + G_b)^2},$$

We consider fluctuations in scattering on surface potential roughness due to randomly distributed hydroxyl groups on NW surface

<sup>v</sup> [Steinhauer&, APL, 107(2015)122112]

# Higher order statistics-bispectrum



- special fingerprints of different gases in bispectra  $S_{3x}(f_1, f_2) = \gamma_{3u}H(f_1)H(f_2)H^*(f_1 + f_2)$ 

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# **FES concept summary**



Based on [Kwan& I3E Sens.J.,8(2008)706]: simplified + extended/updated \*Tulzer&, Nanotechnology 24(2013)315501

## Precautions: What do we really measure?

- Defined measurement conditions:
- surface degasing prior to measurements
- besides measurement of frequency spectra, recording/analysis of time domain waveforms is strongly suggested
  - Not to misinterprete e.g. contact RTS noise as A/D noise
  - Stationarity: Drifts  $\rightarrow$  1/f2 dependence
  - $\rightarrow$  Air and temperature fluctuations in measurement chamber and at the DUT should be low (laminar flow),  $[dT(t) \rightarrow dR(t)]$
- Spectral responses of different gases in a mixture are often not additive (training algorithm necessary) [Solis& I3E Sens.J.,5(2005,1338]
- Be careful in interpretations: even the noise mechanisms in "standard" electronic elements like resistors, FET, BJT,... are still in discussion  $\rightarrow$  effects on sensor optimization strategy 18 DOPERATION IN SCIENCE AND TECHNOLOGY

## Conclusions

- Lorentzian-like and 1/f spectra can be used for gas sensing → additional information to <R> or <R>(t)
- Pure adsorption desorption noise is not yet experimentally demonstrated in frequency domain
- Noise mechanisms in gas sensors are far from being understood!
- Precautions on measurements conditions



#### **Noise measurements**



#### **Supplement to 1/f noise in CuO NWs**

$$\frac{S_R}{R^2} = \frac{S_{Gs} + S_{Gb}}{G^2} = \frac{\frac{\alpha_s}{N_s f} G_s^2 + \frac{\alpha_b}{N_b f} G_b^2}{(G_s + G_b)^2} = \frac{K_s G_s + K_b G_b}{fL^2 (G_s + G_b)^2},$$
$$\frac{K_b G_b + K_s G_s}{(G_b + G_s)^2} = \frac{K_b}{(G_b + G_s)} + \frac{G_s (K_s - K_b)}{(G_b + G_s)^2} = K_b R_{TOT} + G_s (K_s - K_b) R_{TOT}^2$$

$$\frac{1}{N_{s(b)}} = \frac{q\mu_{s(b)}R_{s(b)}}{L^2}$$

Ns(b): number of carriers in the surface (bulk) regions of NW µ-mobilities Ks(b)-coefficients f-frequency Gs(b)-surface (bulk) component of the conductance RTOT=1/GTOT-total resistance

#### **Test system**



- Temperatures up to 350°C - Gas cell with controlled gas flow

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# **Bispectrum**

[- axial symmetry of spectra → stationary process
- magnitude is near zero → the non zero values is due to a weak non-Gaussian component in the amplitude distribution]

An important tool to investigate the non-Gaussian component of the stochastic sensor signal is the bispectrum<sup>10-11</sup>. The bispectrum function is the second-order Fourier transform of the Sens.J.,8(2008)706 third–order cummulant<sup>11</sup>:

$$S_{3x}(f_1, f_2) = \sum_{k=-\infty}^{\infty} \sum_{l=-\infty}^{\infty} C_{3x}(k, l) e^{-j2\pi f_1 k} e^{-j2\pi f_2 l}$$

where  $C_{3x}(k,l) = E[x(n)x(n+k)x(n+l)]$  is the third-order cummulant of the zero-mean process x(n). The bispectrum is a two-dimensional complex function. Usually, its absolute value is analyzed, which is a three-dimensional landscape. The bispectrum function is equal to zero for processes with zero skewness, i.e. for Gaussian processes. The bispectrum of two statistically independent random processes equals the sum of the bispectra of the individual random processes. It is an important property of bispectra that Gaussian components in the recorded stochastic process are eliminated and only the non-Gaussian component are seen<sup>11</sup>.  $S_{2x}(f) = \gamma_{2x} |H(f)|$ 

#### [Smulko&, Sensors and Materials 16(2004)291]

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$$S_{2x}(f) = \gamma_{2u} |H(f)|^2$$

$$S_{3x}(f_1, f_2) = \gamma_{3u} H(f_1) H(f_2) H^*(f_1 + f_2)$$
(9)

where H(f) is the frequency response. It can be seen from (8) and (9) that the power spectrum does not carry any information about the phase of H(f), while if u(n) is non-Gaussian, the phase information can be recovered with the bispectrum.

(4)